

and therefore

$$\begin{aligned} \tan \alpha \int_{v_0}^{v_1} \frac{d}{dv} \left\{ \frac{\Delta(v) \cot v}{1 + \cot^2 \alpha \sin^2 v} \right\} dv \\ = - \int_{v_0}^{v_1} \frac{\Delta(v) \tan \alpha}{(1 + \cot^2 \alpha \sin^2 v) \sin^2 v} dv - K_2 - K_3 \\ = -K_1' - K_2 - K_3, \end{aligned}$$

say. The equation therefore becomes

$$K_1 - K_2 - K_3 = -K_1' - K_2 - K_3,$$

that is $K_1 + K_1' = 0$.

This is

$$\int_{v_0}^{v_1} \frac{\Delta(v)}{1 + \cot^2 \alpha \sin^2 v} \left\{ \cot \alpha + \frac{\tan \alpha}{\sin^2 v} \right\} dv = 0;$$

or, neglecting the factor $\tan \alpha$, we have the equation in the form

$$\int_{v_0}^{v_1} \frac{\Delta(v)}{\sin^2 v} dv = 0.$$

5. To evaluate this integral, we now introduce elliptic functions as in the earlier paper. Writing

$$v = \operatorname{am} u,$$

and denoting by u_0 and u_1 the limits corresponding to v_0 and v_1 , we find

$$\int_{u_0}^{u_1} \frac{dn^2 u}{\sin^2 u} du = 0.$$

But

$$\int \frac{dn^2 u}{\sin^2 u} du = k'^2 u - E(u) - \frac{\operatorname{cn} u \operatorname{dn} u}{\sin u},$$

as an indefinite integral; and therefore we have

$$k'^2 u_1 - E(u_1) - \frac{\operatorname{cn} u_1 \operatorname{dn} u_1}{\sin u_1} = k'^2 u_0 - E(u_0) - \frac{\operatorname{cn} u_0 \operatorname{dn} u_0}{\sin u_0},$$

as the equation determining u_1 when u_0 is given.

One remark may be made about this result. Taking

$$\int \frac{dn^2 u}{\sin^2 u} du = f(u),$$

we have $df(u)/du$ a positive quantity, so that $f(u)$ is continually increasing as u increases; yet the equation gives $f(u_1) = f(u_0)$. The explanation is that $f(u)$ passes through an infinite value—at $u = 2K$ —and changes its sign from positive to negative; it then begins to increase again from $-\infty$.

The equation can be taken in the form

$$\begin{aligned} k'^2(u_1 - u_0) &= E(u_1) - E(u_0) - \left(\frac{\operatorname{cn} u_0 \operatorname{dn} u_0}{\sin u_0} - \frac{\operatorname{cn} u_1 \operatorname{dn} u_1}{\sin u_1} \right) \\ &= E(u_1 - u_0) - k'^2 \operatorname{sn} u_1 \operatorname{sn} u_0 \operatorname{sn}(u_1 - u_0) \\ &\quad - \frac{\operatorname{sn}(u_1 - u_0)}{\operatorname{sn} u_1 \operatorname{sn} u_0} (1 - k'^2 \operatorname{sn}^2 u_1 \operatorname{sn}^2 u_0) \\ &= E(u_1 - u_0) - \frac{\operatorname{sn}(u_1 - u_0)}{\operatorname{sn} u_1 \operatorname{sn} u_0}; \end{aligned}$$

and therefore finally

$$\operatorname{sn}(u_1 - u_0) = \{E(u_1 - u_0) - k'^2(u_1 - u_0)\} \operatorname{sn} u_1 \operatorname{sn} u_0$$

is the equation to determine u_1 . It is evidently satisfied by $u_1 = u_0$; the required value of u_1 is the root of the equation next greater than u_0 .

If preferred, the Zeta-function can be used instead of the second elliptic integral. For any argument, we have

$$Z(u) = E(u) - \frac{E}{K} u,$$

and, therefore,

$$\begin{aligned} E(u) - k'^2 u &= Z(u) + \frac{E - k'^2 K}{K} u \\ &= Z(u) + \frac{G}{K} u, \end{aligned}$$

where G is the quantity introduced by Glaisher.* The equation thus becomes

$$\begin{aligned} \frac{\operatorname{sn}(u_1 - u_0)}{\operatorname{sn} u_1 \operatorname{sn} u_0} &= E(u_1 - u_0) - k'^2(u_1 - u_0) \\ &= Z(u_1 - u_0) + \frac{G}{K}(u_1 - u_0) \\ &= Z(u_1 - u_0) + \frac{2cc'}{K} \frac{dK}{dc}(u_1 - u_0). \end{aligned}$$

* *Quart. Journal*, Vol. XIX. (1883), pp. 145–157; *ib.*, Vol. XX. (1886), pp. 313–361.

6. Taking the equation in the form

$$\operatorname{sn}(u_1 - u_0) = \operatorname{sn} u_1 \operatorname{sn} u_0 \{E(u_1 - u_0) - c'(u_1 - u_0)\},$$

we at once see that

$$\text{if } u_0 = 0, \quad \text{then } u_1 = 2K,$$

$$\text{and if } u_0 = 2K, \quad \text{then } u_1 = 4K.$$

On account of the symmetrical undulation of the geodesic, it is sufficient to take into account values of u_0 , such that

$$0 < u_0 < 2K,$$

in addition to the two limiting values already mentioned.

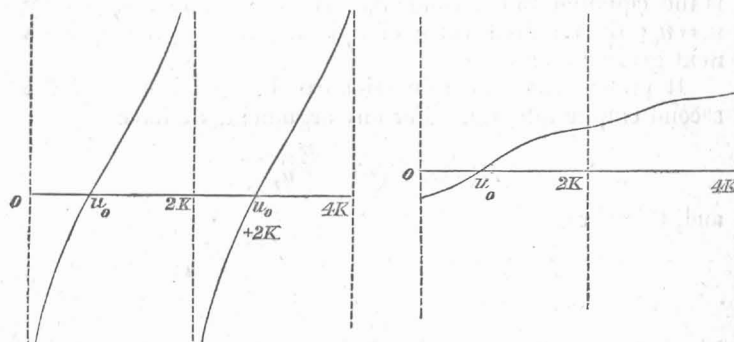
If we consider the curves,

$$y_1 = \frac{\operatorname{sn}(x - u_0)}{\operatorname{sn} x \operatorname{sn} u_0}, \quad y_2 = E(x - u_0) - c'(x - u_0),$$

the first value of x increasing from u_0 , for which $y_1 = y_2$, is u_1

Fig. 1

Fig. 2



Now these curves, when traced, are as in figures 1 and 2 respectively; hence

$$u_0 + 2K < u_1 < 4K.$$

$$\text{If we take } u_1 - u_0 = 2K + \theta_1,$$

$$\text{so that } 0 < \theta_1 < 2K - u_0,$$

$$\text{we have } y_1 = \frac{\operatorname{sn}(2K + \theta_1)}{\operatorname{sn}(2K + u_0 + \theta_1) \operatorname{sn} u_0}$$

$$= \frac{\operatorname{sn} \theta_1}{\operatorname{sn}(u_0 + \theta_1) \operatorname{sn} u_0},$$

$$y_2 = 2G + E(\theta_1) - c'\theta_1;$$

and θ_1 is determined, between the above limits by the equation

$$\frac{\operatorname{sn} \theta_1}{\operatorname{sn}(u_0 + \theta_1) \operatorname{sn} u_0} = 2G + E(\theta_1) - c'\theta_1.$$

7. When the ellipticity of the oblate spheroid is small, c is small. Then G is small; and as

$$E(\theta_1) - c'\theta_1 = c \int_0^{\theta_1} \operatorname{cn}^2 u \, du,$$

it follows that $\operatorname{sn} \theta_1$ (and therefore θ_1) is small of the same order as c . Consequently $E(\theta_1) - c'\theta_1$ is of the second order in c ; also

$$G = 2cc' \frac{dK}{dc} \\ = \frac{1}{4}\pi c,$$

so far as regards the most important term. Hence, when second powers of the ellipticity (and therefore second powers of c) are negligible, we have

$$\theta_1 = \frac{1}{2}\pi c \operatorname{sn}^2 u_0,$$

and consequently the excess of $u_1 - u_0$ above π is

$$\frac{1}{4}\pi c (1 + 2 \operatorname{sn}^2 u_0)$$

to the first order of small quantities.

8. In what precedes, it has been assumed that the geodesic is not a meridian. The special case in which it is a meridian is given by $\alpha = 0$ and then $k^2 = e^2$; so that the preceding formulæ apply on the understanding that the modulus of the elliptic functions is e^2 instead of

$$\frac{e^2 \cos^2 \alpha}{1 - e^2 \sin^2 \alpha}.$$

In particular, when $u_0 = 0$ the conjugate is given by $u_1 = 2\pi$ or $\theta = \pi$: that is, the conjugate of either pole is the other pole—a result to be expected.

25 January, 1896.